# **Subsolidus, high temperature phase relations in**  the systems  $Al_2O_3$ -Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>, MgO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> and MgO-AI<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>

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In the temperature range 1600 to 1900°C, the system  $Al_2O_3-Cr_2O_3-ZrO_2$  is characterized by the coexistence of ZrO<sub>2</sub> (unstablilized) and an (AI, Cr)<sub>2</sub>O<sub>3</sub> solid solution series. In the systems MgO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> and MgO-AI<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> a nearly stoichiometric spinel coexists with both stabilized and unstabilized ZrO<sub>2</sub>. At temperatures above 1600°C a new ternary Mg-AI-Zr oxide becomes stable in the MgO-rich part of the MgO-AI<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> system.

# **1. Introduction**

 $ZrO<sub>2</sub>$  in its various polymorphic forms, stabilized  $ZrO_2$ , and oxide spinels  $(R^{2+}R^{3+} {}_{2}O_4, R^{2+} = Mg,$  $Fe<sup>2+</sup>$ ,  $R<sup>3+</sup> = Al$ ,  $Cr$ ,  $Fe<sup>3+</sup>$ ) are important constituents of many refractory materials, due to their specific properties such as high melting points and chemical inertness. The system  $MgO-Al_2O_3 Cr_2O_3$ - $ZrO_2$ , therefore, represents a convenient starting point for the study of spinel-zirconia ceramics and their properties. To achieve this goal, knowledge of the subsolidus phase relations, including the miscibility of the phases, is essential. The present paper deals with the phase relationships on three of the four limiting ternary systems of the above quaternary, in the relevant temperature range 1600 to  $1900^{\circ}$  C. For details of the experiments and a complete listing of results see [1].

# **2. Previous work**

According to [2] the system  $Al_2O_3$ -Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> is characterized, at temperatures close to the solidus, by the coexistence of unstabilized  $ZrO<sub>2</sub>$  (u-ZrO<sub>2</sub>) with members of the solid solution series  $Al_2O_3-Cr_2O_3$  in all ternary compositions. The join  $MgCr_2O_4-ZrO_2$  of the  $MgO-Cr_2O_3-ZrO_2$  system has been described as a simple eutectic subsystem  $(T_E = 2005 \pm 15^{\circ} \text{C},$ 43 mol %  $ZrO_2$ ) by [3], with mutual solid solubilities of approximately 4 and 3 mol% of the  $ZrO<sub>2</sub>$  and spinel phase, respectively. In the  $MgAl_2O_4-ZrO_2$  system no ternary compound has been encountered either [4-6] and solid solubility is very restricted [4]. A new high temperature phase in the MgO-rich part of the  $MgO-Al_2O_3-ZrO_2$  system has been reported by [7] and independently by [8].

# **3. Experimental procedure**

Starting materials were prepared from appropriate amounts of fine-grained (less than 50  $\mu$ m) pure oxides, MgO, (Merck lot no. 5865),  $Al_2O_3$  (Alcoa A17), Cr<sub>2</sub>O<sub>3</sub>

(Bayer) and monoclinic  $ZrO<sub>2</sub>$  (Dynamit-Nobel, MS 0 to 10  $\mu$ m), taking the absorbed water content into account. These materials were thoroughly mixed in a corundum ball mill for 2 h with ethanol, cold pressed in an impact press into cylinders (50mm diameter, 50 mm high) and dried at  $100^{\circ}$  C for 24 h. The cylinders were heated isothermally at 1600, 1700, 1800 and 1900  $\pm$  15°C under oxidizing conditions in a gas-air heated combustion furnace for 6 to 24h, and then cooled to room temperature. All bulk specimens containing  $Cr_2O_3$  have been analysed by X-ray fluorescence to check for loss of  $Cr_2O_3$  through volatilization during heating. Phases present in the products were identified from powder X-ray diffractograms and their composition was derived from the lattice parameters (for Mg-Al-spinels [9, 10], for Mg-Cr-spinels [11, 12] and for  $(Al, Cr)<sub>2</sub>O<sub>3</sub>$  [13]), and, in some cases, by microprobe analysis.

# **4. Results**

Two forms of  $ZrO<sub>2</sub>$ -rich phases have been observed in the products: monoclinic  $ZrO_2$  (m- $ZrO_2$ ), chemically

TABLE I Representative results on the system  $Al_2O_3-Cr_2O_3 ZrO<sub>2</sub>$  at 1800°C, 24h

Bulk composition		Lattice constants (Al.	
Planned	Measured	$Cr$ , $O_3$ phase	
		$a$ (nm)	$c$ (nm)
40.0/15.0/45.0	40.2/14.7/45.1	$0.4822(1)$ <sup>†</sup>	1.3153(3)
33.3/33.3/33.3	33.5/33.1/33.4	0.4868(1)	1.3283(6)
15.0/40.0/45.0	15.0/39.8/45.2	0.4911(1)	1.3425(1)
20.0/20.0/60.0	20.1/20.0/59.9	0.4868(1)	1.3288(5)

m-ZrO<sub>2</sub> lattice constants were in the ranges  $a = 0.5145 - 0.5152$  nm,  $b = 0.5201 - 0.5207$  nm,  $c = 0.5317 - 0.5320$  nm,  $\beta = 99^{\circ}5' - 99^{\circ}12'$ . \*The product phase assemblage is monoclinic  $ZrO_2$  (m- $ZrO_2$ ) + (Al,  $Cr_2O_3$  throughout. Chemical compositions (in mol%) are given in the form  $\text{Al}_2\text{O}_3/\text{Cr}_2\text{O}_3/\text{ZrO}_2$ .

<sup>†</sup>Parenthesized figures represent estimated standard deviations in units of the figure quoted to their immediate left.

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TABLE II Representative results on the system MgO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> at 1800<sup>o</sup>C, 24h

Products
m-ZrO <sub>2</sub> , PC ( $a = 0.83332(5)$ )
m-ZrO <sub>2</sub> , PC ( $a = 0.83327(3)$ )
c-ZrO, $(a = 0.5072(1))$ , PC $(a = 0.83365(2))$ , MgO
c-ZrO <sub>2</sub> (a = 0.5071 (1)), PC (a = 0.83350 (11)), MgO
m-ZrO <sub>2</sub> , PC ( $a = 0.83330(3)$ )
m-ZrO <sub>2</sub> , $(a = 0.83376(3))$ , Cr <sub>2</sub> O <sub>3</sub>

\*Chemical compositions (in mol %) are given in the form  $MgO/Cr_2O_3/ZrO_2$ .  $PC =$  picochromite, close to  $MgCr_2O_4$ .  $a =$  lattice constants (in nm).

tParenthesized figures represent estimated standard deviations in units of the figure quoted to their immediate left.

close to pure  $ZrO_2$ , and cubic  $ZrO_2$  (c-ZrO<sub>2</sub>) which is the form stabilized through significant amounts of MgO. In the temperature range studied here, m- $ZrO<sub>2</sub>$ is unstable, and it results in the products from inversion from a probably tetragonal high temperature phase [14]. In discussing the phase relations at high temperature, we will, therefore, use the term  $u$ -ZrO, for the unstabilized form of  $ZrO<sub>2</sub>$ .

# 4.1. The system  $Al_2O_3-Cr_2O_3-ZrO_2$

In agreement with [2], only the two-phase assemblage  $u-ZrO<sub>2</sub> + (Al, Cr)<sub>2</sub>O<sub>3</sub>$  solid solution has been encountered in the entire temperature range studied. A heat treatment of 24 h duration is sufficient to produce, from the starting materials, a homogeneous (AI,  $Cr$ <sub>2</sub>O<sub>3</sub> phase. Chemical analyses of the bulk products (Table I) as well as the lattice constants of the (A1,  $Cr$ <sub>2</sub>O<sub>3</sub> phase indicate that loss of chromium during heating is negligible. From microprobe analyses it is inferred that the  $ZrO_2$  content of the  $(A1, Cr)_2O_3$  phase is less than  $2 \times v'$ , and no indications for a solubility of (Al,  $Cr_2O_3$  in  $ZrO_2$  could be derived from the lattice constants of the latter phase.

#### 4.2. The system  $MgO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>$

Results are tabulated in Table II and the subsolidus phase diagram is depicted in Fig. 1. The topology of the system remains unchanged in the temperature range studied: it is subdivided by two two-phase fields,



u-ZrO<sub>2</sub> + spinel and c-ZrO<sub>2</sub> + spinel, so that three three-phase fields appear. At a MgO :  $Cr_2O_3$  ratio of 1 (i.e. on the join  $ZrO_2-MgCr_2O_4$ ) only u-ZrO<sub>2</sub> and a stoichiometric spinel can coexist, whereas formation of c-ZrO<sub>2</sub> requires an excess of MgO over  $Cr_2O_3$ . It should be noted that the assemblage spinel  $+ u$ -ZrO<sub>2</sub> + c-ZrO<sub>2</sub> is stable only over a very narrow range of  $MgO: Cr<sub>2</sub>O<sub>3</sub>$  ratio.

Upon increasing temperature from 1600 to 1900 $^{\circ}$ C the solid solution ranges of both the  $c$ - $ZrO$ , and spinel phase increase slightly and consequently the twophase fields widen systematically.

#### 4.3. The system  $MgO-AI_2O_3-ZrO_2$

At 1600°C no ternary compound has been observed, and the topology of the system is identical to that found for the  $MgO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>$  system (Table III). The only difference is the larger solubility of the Mg-Al-spinel, particularly towards  $Al_2O_3$  (Fig. 2a). Again, when MgO:  $Al_2O_3 = 1$ , u-ZrO<sub>2</sub> coexists with a nearly stoichiometric MgAl<sub>2</sub>O<sub>4</sub> spinel. The c-ZrO<sub>2</sub> +  $u-ZrO<sub>2</sub> + spinel$  assemblage is restricted, at 26.6 mol %  $ZrO_2$  component, to  $MgO: Al_2O_3$  ratios above 1 and less than 1.14.

In the temperature range 1600 to  $1700^{\circ}$ C a ternary compound becomes stable in the MgO-rich part of the system [8, 15] which seems to be identical to that reported independently by [7]. Its composition depends slightly on the bulk composition,

*Figure 1* Section through the system  $MgO - Cr<sub>2</sub>O<sub>3</sub>$  $ZrO<sub>2</sub>$  at 1800°C. Abbreviations: u-ZrO<sub>2</sub> = unstabilized  $ZrO_2$ , c-ZrO<sub>2</sub> = cubic (stabilized) ZrO<sub>2</sub>, PC = picochromite, close to MgCr<sub>2</sub>O<sub>4</sub>. Bulk compositions investigated are indicated by crosses. Two-phase fields originating from the small

TABLE III Representative results on the system MgO-Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> at 1600 and 1800<sup>o</sup>C

Bulk composition	Products			
	$1600^{\circ}$ C	$1800^{\circ}$ C		
36.5/36.5/27.0	Sp ( $a = 0.80830$ (6)), m-ZrO <sub>2</sub>	Sp ( $a = 0.80823$ (8)), m-ZrO,		
23.0/47.0/30.0	Sp (a = 0.80081 (9)), m-ZrO <sub>2</sub> , Cor	Sp ( $a = 0.80065$ (8)), m-ZrO <sub>2</sub>		
50.0/26.0/24.0	Sp (a = 0.80889 (7)), c-ZrO <sub>2</sub> (a = 0.5079 (1)), MgO	Sp (a = 0.80876 (5)), c-ZrO, (a = 0.5083 (1)), MgO, X		
57.8/10.6/31.6	$Sp, c-ZrO, MgO$	Sp. c- $ZrO_2$ , MgO, X		
38.4/35.0/26.6	$Sp, c-ZrO2, m-ZrO2$	$Sp, c-ZrO, m-ZrO,$		
39.1/34.3/26.6	$Sp, c-ZrO,$	$Sp, c-2rO,$		
36.0/35.5/28.5	$Sp, c-ZrO, m-ZrO,$	$Sp, c-ZrO, m-ZrO,$		

\*Chemical compositions (in mol %) are given in the form  $MgO/Al_2O_3/ZrO_2$ . Sp = spinel, Cor = corundum. X = ternary  $Mg-Al-Zr$  oxide.  $a =$  lattice constants (in nm), with their estimated standard deviations.

temperature and run duration. 100% yields of this phase could not be achieved, it always coexisted with minor amounts of relic c- $ZrO<sub>2</sub>$ , MgO, and spinel. The microprobe analyses define a chemical variation of the phase that may be described by a formula  $Mg_{5+x}Al_{2,4-x}Zr_{1.7+0.25x}O_{12}$  with  $-0.4 \le x \le 0.4$ (Fig. 3). Through the existence of this phase, the c-ZrO<sub>2</sub> + MgO + spinel three-phase field in the  $1600^{\circ}$  C section is further subdivided under equilibrium conditions into three different three-phase fields involving the ternary compound at temperatures of and above  $1700^{\circ}$  C. When the ternary compound is hot annealed at or slightly below  $1600^{\circ}$ C, it decomposes within about 2h to the metastable assemblage  $MgO + c-ZrO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  (corundum) which only subsequently is transformed to MgO  $+$  $MgA1_2O_4 + c-ZrO_2$ . Temperature increase beyond  $1700^{\circ}$ C leads to an expansion of the twophase fields c- $ZrO<sub>2</sub>$  + spinel and u- $ZrO<sub>2</sub>$  + spinel (Fig. 2b).



*Figure2* Sections through the system MgO  $Al_2O_3-ZrO_2$  at (a) 1600°C and (b) 1800°C. Abbreviations:  $u-ZrO_2 =$  unstabilized  $ZrO_2$ ,  $c-ZrO<sub>2</sub> = cubic$  (stabilized)  $ZrO<sub>2</sub>$ , Sp = magnesium aluminate spinel,  $X =$  ternary  $Mg-A$ 1-Zr-oxide (cf. text). Compositions investigated are indicated by crosses. Two-phase fields originating from the small solid solubilities of u-ZrO<sub>2</sub>, MgO, X, and  $Al_2O_3$  are omitted for simplicity.



*Figure 3* Results of microprobe analyses of the new ternary compound X in part of the system MgO-Al<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> (in mol%). Synthesis conditions: 1800°C, 24 h slow cooling (crosses); 1800°C, 48 h, fast quench (small dots). The dashed line indicates the chemical variability according to the formula  $Mg_{5+x}Al_{24-x}Zr_{1.7+0.25x}O_{12}$ . Specific compositions corresponding to  $x = -0.4$ , 0, and  $+0.4$  are given by dots labelled 1, 2, 3, respectively. The open circle represents the composition of the phase reported by Firatli [7].

# **5. Discussion**

In all the systems studied, solidus temperatures are above  $1900^{\circ}$ C which is one of the prerequisites for their usefulness as materials of refractories.

 $c$ -ZrO<sub>2</sub> can only be formed in the presence of excess MgO over Al<sub>2</sub>O<sub>3</sub> or Cr<sub>2</sub>O<sub>3</sub>. For the binary systems  $ZrO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>$  and  $ZrO<sub>2</sub>-Cr<sub>2</sub>O<sub>3</sub>$  the eutectoid temperature marking the decomposition of  $c$ -ZrO<sub>2</sub> into the respective oxides lies at too high temperatures (probably slightly below  $2000^{\circ}$  C [16]). We cannot exclude that in the 1900 $^{\circ}$ C runs c-ZrO<sub>2</sub> has been present during sintering even when  $MgO:(Al<sub>2</sub>O<sub>3</sub>)$ ,  $Cr<sub>2</sub>O<sub>3</sub>$ ) was below 1 but that this phase decomposed during cooling because of the rapid kinetics close to the high eutectold temperature, and the rather poor thermal conductivity of  $ZrO<sub>2</sub>$ . In the  $ZrO<sub>2</sub>$ -MgO system the eutectoid temperature of the c- $ZrO<sub>2</sub>$  decomposition is in the vicinity of  $1400^{\circ}$  C [16].

Refractories based only on spinel phases suffer from poor resistance to thermal shock. This property might be improved particularly through coexisting c-ZrO<sub>2</sub> +  $u-ZrO<sub>2</sub>$  (partially stabilized zirconia), and the phase relations obtained here indicate that a spinel + c-ZrO<sub>2</sub> + u-ZrO<sub>2</sub> assemblage can only be produced at  $MgO:(Al, Cr)<sub>2</sub>O<sub>3</sub>$  ratios slightly above 1 (Figs 1 and 2). The ternary phase in the  $MgO-AI_2O_3-ZrO_2$  system is about 10% less dense than c-ZrO<sub>2</sub> + MgAl<sub>2</sub>O<sub>4</sub> + MgO, and its presence in a refractory would induce severe strain as soon as the lower stability limit of the phase (between 1600 and 1700 $^{\circ}$ C) is reached.

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