Subsolidus, high temperature phase relations in the systems Al_2O_3 - Cr_2O_3 - ZrO_2 , MgO- Cr_2O_3 - ZrO_2 and MgO- Al_2O_3 - ZrO_2

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In the temperature range 1600 to 1900° C, the system $AI_2O_3 - Cr_2O_3 - ZrO_2$ is characterized by the coexistence of ZrO_2 (unstabilized) and an (AI, $Cr)_2O_3$ solid solution series. In the systems $MgO-Cr_2O_3-ZrO_2$ and $MgO-AI_2O_3-ZrO_2$ a nearly stoichiometric spinel coexists with both stabilized and unstabilized ZrO_2 . At temperatures above 1600° C a new ternary Mg-AI-Zr oxide becomes stable in the MgO-rich part of the $MgO-AI_2O_3-ZrO_2$ system.

1. Introduction

ZrO₂ in its various polymorphic forms, stabilized ZrO_2 , and oxide spinels $(R^{2+}R^{3+}O_4, R^{2+} = Mg)$, Fe^{2+} , $R^{3+} = Al$, Cr, Fe^{3+}) are important constituents of many refractory materials, due to their specific properties such as high melting points and chemical inertness. The system MgO-Al₂O₃- Cr_2O_3 -ZrO₂, therefore, represents a convenient starting point for the study of spinel-zirconia ceramics and their properties. To achieve this goal, knowledge of the subsolidus phase relations, including the miscibility of the phases, is essential. The present paper deals with the phase relationships on three of the four limiting ternary systems of the above quaternary, in the relevant temperature range 1600 to 1900° C. For details of the experiments and a complete listing of results see [1].

2. Previous work

According to [2] the system Al₂O₃-Cr₂O₃-ZrO₂ is characterized, at temperatures close to the solidus, by the coexistence of unstabilized ZrO₂ (u-ZrO₂) with members of the solid solution series Al₂O₃-Cr₂O₃ in all ternary compositions. The join MgCr₂O₄-ZrO₂ of the MgO-Cr₂O₃-ZrO₂ system has been described as a simple eutectic subsystem ($T_E = 2005 \pm 15^{\circ}$ C, 43 mol % ZrO₂) by [3], with mutual solid solubilities of approximately 4 and 3 mol % of the ZrO₂ and spinel phase, respectively. In the MgAl₂O₄-ZrO₂ system no ternary compound has been encountered either [4-6] and solid solubility is very restricted [4]. A new high temperature phase in the MgO-rich part of the MgO-Al₂O₃-ZrO₂ system has been reported by [7] and independently by [8].

3. Experimental procedure

Starting materials were prepared from appropriate amounts of fine-grained (less than 50 μ m) pure oxides, MgO, (Merck lot no. 5865), Al₂O₃ (Alcoa A17), Cr₂O₃

(Bayer) and monoclinic ZrO₂ (Dynamit-Nobel, MS 0 to 10 μ m), taking the absorbed water content into account. These materials were thoroughly mixed in a corundum ball mill for 2h with ethanol, cold pressed in an impact press into cylinders (50 mm diameter, 50 mm high) and dried at 100° C for 24 h. The cylinders were heated isothermally at 1600, 1700, 1800 and $1900 \pm 15^{\circ}$ C under oxidizing conditions in a gas-air heated combustion furnace for 6 to 24 h, and then cooled to room temperature. All bulk specimens containing Cr2O3 have been analysed by X-ray fluorescence to check for loss of Cr₂O₃ through volatilization during heating. Phases present in the products were identified from powder X-ray diffractograms and their composition was derived from the lattice parameters (for Mg-Al-spinels [9, 10], for Mg-Cr-spinels [11, 12] and for (Al, $Cr_{2}O_{3}$ [13]), and, in some cases, by microprobe analysis.

4. Results

Two forms of ZrO_2 -rich phases have been observed in the products: monoclinic ZrO_2 (m- ZrO_2), chemically

TABLE I Representative results on the system $Al_2O_3-Cr_2O_3-ZrO_2$ at 1800°C, 24 h

Bulk composition		Lattice constants (Al,	
Planned	Measured	$Cr)_2O_3$ phase	
		<i>a</i> (nm)	c (nm)
40.0/15.0/45.0	40.2/14.7/45.1	0.4822 (1) [†]	1.3153 (3)
33.3/33.3/33.3	33.5/33.1/33.4	0.4868 (1)	1.3283 (6)
15.0/40.0/45.0	15.0/39.8/45.2	0.4911 (1)	1.3425 (1)
20.0/20.0/60.0	20.1/20.0/59.9	0.4868 (1)	1.3288 (5)

m-ZrO₂ lattice constants were in the ranges a = 0.5145-0.5152 nm, b = 0.5201-0.5207 nm, c = 0.5317-0.5320 nm, $\beta = 99^{\circ}5'-99^{\circ}12'$. *The product phase assemblage is monoclinic ZrO₂ (m-ZrO₂) + (Al, Cr)₂O₃ throughout. Chemical compositions (in mol%) are given in the form Al₂O₃/Cr₂O₃/ZrO₂.

[†]Parenthesized figures represent estimated standard deviations in units of the figure quoted to their immediate left.

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TABLE II Representative results on the system MgO-Cr₂O₃-ZrO₂ at 1800°C, 24 h

Bulk composition		Products
Planned	Measured	
33.5/33.5/33.0*	33.5/33.4/33.1	$m-ZrO_2$, PC ($a = 0.83332$ (5))
40.0/40.0/20.0	40.1/40.3/19.5	m-ZrO ₂ , PC ($a = 0.83327$ (3))
55.0/23.0/22.0	54.7/23.1/22.2	$c-ZrO_2$ (a = 0.5072 (1)), PC (a = 0.83365 (2)), MgO
43.5/28.5/28.0	44.0/28.5/27.5	$c-ZrO_2$ (a = 0.5071 (1)), PC (a = 0.83350 (11)), MgO
25.0/25.0/50.0	24.9/25.3/49.8	m-ZrO ₂ , PC ($a = 0.83330$ (3))
25.0/38.0/37.0	24.9/38.0/37.1	$m-ZrO_2$, $(a = 0.83376 (3))$, Cr_2O_3

* Chemical compositions (in mol %) are given in the form MgO/Cr₂O₃/ZrO₂. PC = picochromite, close to MgCr₂O₄. a = lattice constants (in nm).

[†]Parenthesized figures represent estimated standard deviations in units of the figure quoted to their immediate left.

close to pure ZrO_2 , and cubic ZrO_2 (c- ZrO_2) which is the form stabilized through significant amounts of MgO. In the temperature range studied here, m- ZrO_2 is unstable, and it results in the products from inversion from a probably tetragonal high temperature phase [14]. In discussing the phase relations at high temperature, we will, therefore, use the term u- ZrO_2 for the unstabilized form of ZrO_2 .

4.1. The system $Al_2O_3 - Cr_2O_3 - ZrO_2$

In agreement with [2], only the two-phase assemblage $u-ZrO_2 + (Al, Cr)_2O_3$ solid solution has been encountered in the entire temperature range studied. A heat treatment of 24 h duration is sufficient to produce, from the starting materials, a homogeneous (Al, $Cr)_2O_3$ phase. Chemical analyses of the bulk products (Table I) as well as the lattice constants of the (Al, $Cr)_2O_3$ phase indicate that loss of chromium during heating is negligible. From microprobe analyses it is inferred that the ZrO_2 content of the (Al, $Cr)_2O_3$ phase is less than 2 wt %, and no indications for a solubility of (Al, $Cr)_2O_3$ in ZrO_2 could be derived from the lattice constants of the latter phase.

4.2. The system MgO- Cr_2O_3 -ZrO₂

Results are tabulated in Table II and the subsolidus phase diagram is depicted in Fig. 1. The topology of the system remains unchanged in the temperature range studied: it is subdivided by two two-phase fields,



u-ZrO₂ + spinel and c-ZrO₂ + spinel, so that three three-phase fields appear. At a MgO : Cr_2O_3 ratio of 1 (i.e. on the join $ZrO_2-MgCr_2O_4$) only u-ZrO₂ and a stoichiometric spinel can coexist, whereas formation of c-ZrO₂ requires an excess of MgO over Cr_2O_3 . It should be noted that the assemblage spinel + u-ZrO₂ + c-ZrO₂ is stable only over a very narrow range of MgO : Cr_2O_3 ratio.

Upon increasing temperature from 1600 to 1900° C the solid solution ranges of both the c-ZrO₂ and spinel phase increase slightly and consequently the two-phase fields widen systematically.

4.3. The system MgO-Al₂O₃-ZrO₂

At 1600° C no ternary compound has been observed, and the topology of the system is identical to that found for the MgO-Cr₂O₃-ZrO₂ system (Table III). The only difference is the larger solubility of the Mg-Al-spinel, particularly towards Al₂O₃ (Fig. 2a). Again, when MgO: Al₂O₃ = 1, u-ZrO₂ coexists with a nearly stoichiometric MgAl₂O₄ spinel. The c-ZrO₂ + u-ZrO₂ + spinel assemblage is restricted, at 26.6 mol % ZrO₂ component, to MgO: Al₂O₃ ratios above 1 and less than 1.14.

In the temperature range 1600 to 1700° C a ternary compound becomes stable in the MgO-rich part of the system [8, 15] which seems to be identical to that reported independently by [7]. Its composition depends slightly on the bulk composition,

Figure 1 Section through the system MgO-Cr₂O₃-ZrO₂ at 1800°C. Abbreviations: u-ZrO₂ = unstabilized ZrO₂, c-ZrO₂ = cubic (stabilized) ZrO₂, PC = picochromite, close to MgCr₂O₄. Bulk compositions investigated are indicated by crosses. Two-phase fields originating from the small solid solubilities of u-ZrO₂, MgO, and Cr₂O₃ are omitted for simplicity.

TABLE III Representative results on the system MgO-Al₂O₃-ZrO₂ at 1600 and 1800°C

Bulk composition	Products			
	1600° C	1800° C		
36.5/36.5/27.0	$Sp (a = 0.80830 (6)), m-ZrO_2$	Sp $(a = 0.80823 (8)), \text{ m-ZrO}_2$		
23.0/47.0/30.0	Sp ($a = 0.80081$ (9)), m-ZrO ₂ , Cor	Sp ($a = 0.80065$ (8)), m-ZrO ₂		
50.0/26.0/24.0	Sp ($a = 0.80889$ (7)), c-ZrO ₂ ($a = 0.5079$ (1)), MgO	Sp ($a = 0.80876$ (5)), c-ZrO ₂ ($a = 0.5083$ (1)), MgO, X		
57.8/10.6/31.6	Sp, $c-ZrO_2$, MgO	Sp, $c-ZrO_2$, MgO, X		
38.4/35.0/26.6	Sp, $c-ZrO_2$, $m-ZrO_2$	Sp, $c-ZrO_2$, $m-ZrO_2$		
39.1/34.3/26.6	Sp, $c-ZrO_2$	Sp, $c-ZrO_2$		
36.0/35.5/28.5	Sp, $c-ZrO_2$, $m-ZrO_2$	Sp, $c-ZrO_2$, $m-ZrO_2$		

*Chemical compositions (in mol %) are given in the form $MgO/Al_2O_3/ZrO_2$. Sp = spinel, Cor = corundum. X = ternary Mg-Al-Zr oxide. a = lattice constants (in nm), with their estimated standard deviations.

temperature and run duration. 100% yields of this phase could not be achieved, it always coexisted with minor amounts of relic c-ZrO₂, MgO, and spinel. The microprobe analyses define a chemical variation of the phase that may be described by a formula $Mg_{5+x}Al_{2.4-x}Zr_{1.7+0.25x}O_{12}$ with $-0.4 \le x \le 0.4$ (Fig. 3). Through the existence of this phase, the c-ZrO₂ + MgO + spinel three-phase field in the 1600°C section is further subdivided under equilibrium conditions into three different three-phase fields

involving the ternary compound at temperatures of and above 1700° C. When the ternary compound is hot annealed at or slightly below 1600° C, it decomposes within about 2h to the metastable assemblage MgO + c-ZrO₂ + Al₂O₃ (corundum) which only subsequently is transformed to MgO + MgAl₂O₄ + c-ZrO₂. Temperature increase beyond 1700° C leads to an expansion of the twophase fields c-ZrO₂ + spinel and u-ZrO₂ + spinel (Fig. 2b).



Figure 2 Sections through the system MgO– Al₂O₃–ZrO₂ at (a) 1600° C and (b) 1800° C. Abbreviations: u-ZrO₂ = unstabilized ZrO₂, c-ZrO₂ = cubic (stabilized) ZrO₂, Sp = magnesium aluminate spinel, X = ternary Mg–Al– Zr-oxide (cf. text). Compositions investigated are indicated by crosses. Two-phase fields originating from the small solid solubilities of u-ZrO₂, MgO, X, and Al₂O₃ are omitted for simplicity.



Figure 3 Results of microprobe analyses of the new ternary compound X in part of the system MgO-Al₂O₃-ZrO₂ (in mol %). Synthesis conditions: 1800° C, 24 h slow cooling (crosses); 1800° C, 48 h, fast quench (small dots). The dashed line indicates the chemical variability according to the formula $Mg_{5+x}Al_{24-x}Zr_{1.7+0.25x}O_{12}$. Specific compositions corresponding to x = -0.4, 0, and +0.4 are given by dots labelled 1, 2, 3, respectively. The open circle represents the composition of the phase reported by Firatli [7].

5. Discussion

In all the systems studied, solidus temperatures are above 1900° C which is one of the prerequisites for their usefulness as materials of refractories.

c-ZrO₂ can only be formed in the presence of excess MgO over Al₂O₃ or Cr₂O₃. For the binary systems $ZrO_2-Al_2O_3$ and $ZrO_2-Cr_2O_3$ the eutectoid temperature marking the decomposition of c-ZrO₂ into the respective oxides lies at too high temperatures (probably slightly below 2000° C [16]). We cannot exclude that in the 1900° C runs c-ZrO₂ has been present during sintering even when MgO: (Al₂O₃, Cr₂O₃) was below 1 but that this phase decomposed during cooling because of the rapid kinetics close to the high eutectoid temperature, and the rather poor thermal conductivity of ZrO₂. In the ZrO₂-MgO system the eutectoid temperature of the c-ZrO₂ decomposition is in the vicinity of 1400° C [16].

Refractories based only on spinel phases suffer from poor resistance to thermal shock. This property might be improved particularly through coexisting $c-ZrO_2 +$ $u-ZrO_2$ (partially stabilized zirconia), and the phase relations obtained here indicate that a spinel + $c-ZrO_2 + u-ZrO_2$ assemblage can only be produced at MgO: (Al, Cr)₂O₃ ratios slightly above 1 (Figs 1 and 2). The ternary phase in the MgO-Al₂O₃-ZrO₂ system is about 10% less dense than $c-ZrO_2 + MgAl_2O_4$ + MgO, and its presence in a refractory would induce severe strain as soon as the lower stability limit of the phase (between 1600 and 1700° C) is reached.

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